

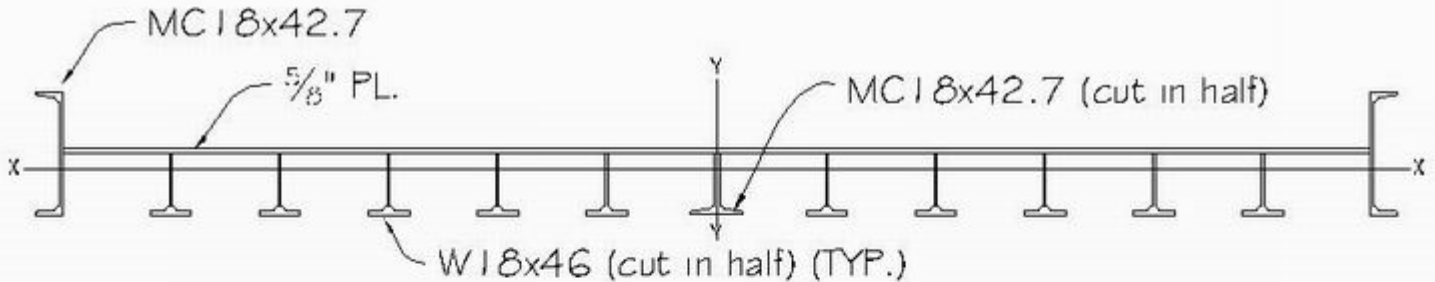
RAMP DESIGN

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April 29, 2010

(DISCLAIMER: This worksheet is shared only as an example and should be used with caution.)
(The calculations are not guaranteed to be error free.)

Define the section modulus for ramp section

(section modulus calculated using AutoCAD, see graphic below)



..... REGIONS

Area:	226.6616 sq in
Perimeter:	833.0722 in
Bounding box:	X: -99.9506 -- 99.9504 in Y: -6.8177 -- 11.1823 in
Centroid:	X: -0.0003 in Y: 0.0000 in
Moments of inertia:	X: 4216.4402 sq in sq in Y: 800704.1645 sq in sq in
Product of inertia:	XY: -0.1510 sq in sq in
Radii of gyration:	X: 4.3130 in Y: 59.4357 in
Principal moments (sq in sq in) and X-Y directions about centroid:	I: 4216.4402 along [1.0000 0.0000] J: 800704.1645 along [0.0000 1.0000]
Elastic section moduli:	
Section modulus (Top)	X: 377.0638
Section modulus (Bottom)	X: 618.4549
Section modulus (Right)	Y: 8011.0151
Section modulus (Left)	Y: 8010.9991

Smod = section modulus (in³)

$$S_{mod} = 377.0638 \text{ in}^3$$

Calculate the maximum allowable stress in tension and compression

σ_u = ultimate tensile strength (ksi)
 σ_y = yield stress (ksi)
 FS = safety factor
 σ_{all} = maximum allowable stress in tension or compression (ksi)

$$ksi := 1000 \text{ psi}$$

$$\sigma_u := 58 \text{ ksi}$$

$$\sigma_y := 36 \text{ ksi}$$

$$FS := 3.0$$

$$\sigma_{all} := \frac{\sigma_y}{FS} \quad \sigma_{all} = 12 \text{ ksi}$$

Calculate the maximum allowable moment

$M_{all} = \text{maximum allowable moment (ft}\cdot\text{lb)}$

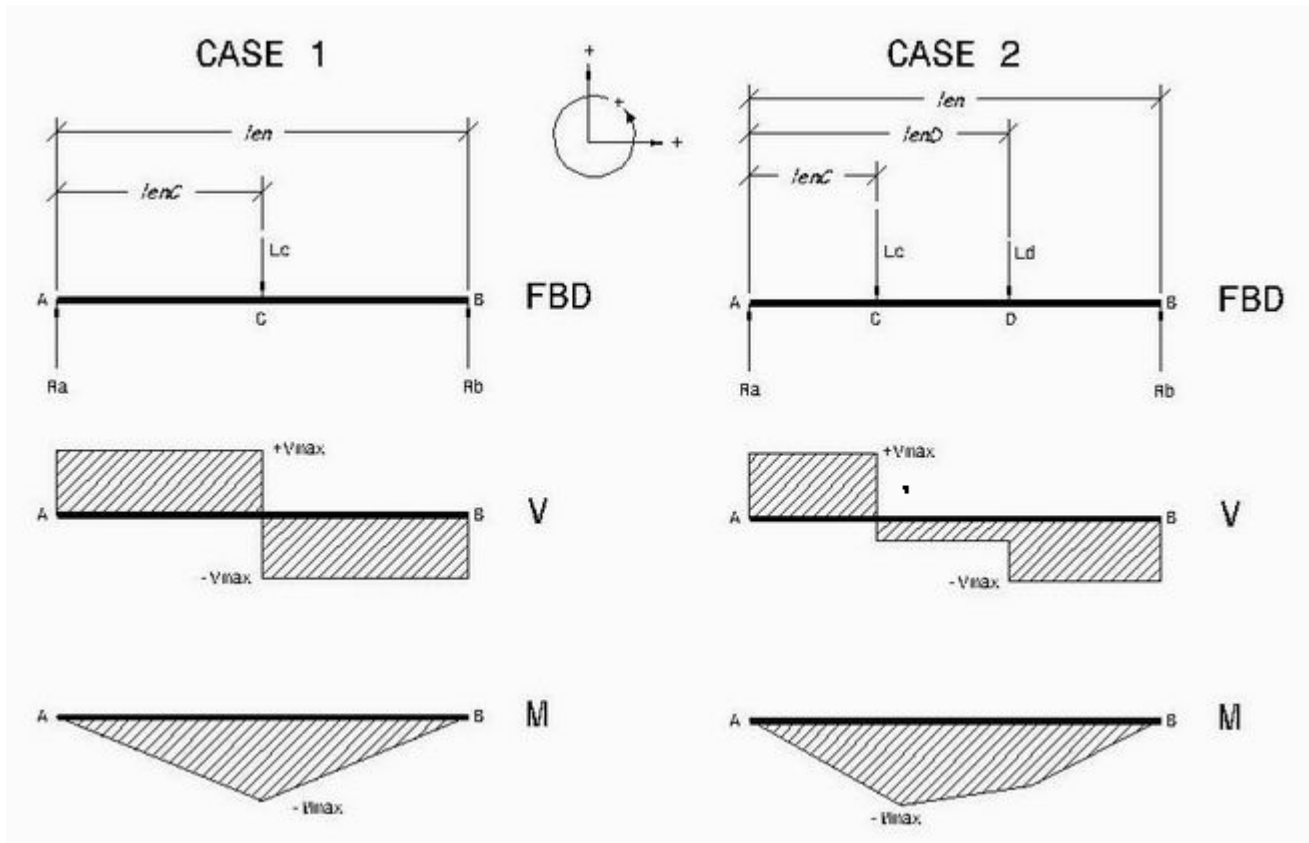
$M_{all} := S_{mod} \cdot \sigma_{all}$

$M_{all} = 3.7706 \cdot 10^5 \text{ ft}\cdot\text{lb}$

FBD, V, and M diagrams

CASE 1 = front axle of large forklift on ramp

CASE 2 = both axles of smaller fully-loaded forklift on ramp



CASE 1: front axle of unloaded large forklift on ramp

Calculate Bending Moment:

len = length of the ramp (ft)
 len_C = distance from A to C, the point of application of Load C (ft)
 L_c = load at C (kips)
 R_b = reaction at B (kips)
 R_a = reaction at A (kips)
 $posV_{max}$ = maximum positive shear (+kips)
 $negV_{max}$ = maximum negative shear (-kips)
 M_{max} = maximum bending moment (ft \cdot lb)

$len := 21 \text{ ft}$

$len_C := 10.5 \text{ ft}$

$L_c := 67.739 \text{ kip}$

Note: actual front axle load for unloaded Hyster H1050HDS

Calculate the reactions at A and B:

$$R_b := \frac{L_c \cdot \text{lenC}}{\text{len}} \quad R_b = 33.8695 \text{ kip}$$

$$R_a := L_c - R_b \quad R_a = 33.8695 \text{ kip}$$

Calculate the maximum shear forces:

$$\text{posVmax} := R_a \quad \text{posVmax} = 33.8695 \text{ kip}$$

$$\text{negVmax} := R_b \quad \text{negVmax} = 33.8695 \text{ kip}$$

Calculate the maximum bending moment:

$$M_{\text{max}} := \text{posVmax} \cdot (\text{lenC})$$

$$M_{\text{max}} = 3.5563 \cdot 10^5 \text{ ft lbf}$$

Compare maximum bending moment to allowable bending moment:

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if Mall > Mmax
  result := "Pass"
else
  result := "Fail"
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result = "Pass"

Calculate Max Deflection:

<p>E = modulus of elasticity (ksi) I = moment of inertia about horizontal centroidal axis (in⁴) ymax = maximum deflection (in)</p>

Define modulus of elasticity and moment of inertia values:

$$E := 29000 \text{ ksi}$$

$$I := 4216.4402 \text{ in}^4$$

Calculate the maximum deflection:

```
if lenC ≤ len/2
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$$y_{\text{max}} := \frac{-L_c \cdot \text{lenC}}{3 \cdot E \cdot I \cdot \text{len}} \cdot \left(\frac{\text{len}^2 - \text{lenC}^2}{3} \right)^{\frac{3}{2}}$$

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else
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$$\text{lenC} := \text{len} - \text{lenC}$$

$$y_{\text{max}} := \frac{-L_c \cdot \text{lenC}}{3 \cdot E \cdot I \cdot \text{len}} \cdot \left(\frac{\text{len}^2 - \text{lenC}^2}{3} \right)^{\frac{3}{2}}$$

<-- Note: lenC must be less than half the total length (len)

ymax = -0.1847 in

CASE 2 : both axles of smaller fully-loaded forklift on ramp

Calculate Bending Moment:

Lc = load at C , which is the larger of the two loads (kips)
 Ld = load at D (kips)
 wheelbase = the distance between the wheels on the forklift (in)
 len = length of the ramp (ft)
 lenC = distance from A to C, the point of application of Load C (ft)
 lenD = distance from A to D, the point of application of Load D (ft)
 Rb = reaction at B (kips)
 Ra = reaction at A (kips)
 posVmax = maximum positive shear (+kips)
 negVmax = maximum negative shear (-kips)
 Mmax = maximum bending moment (ft*lb)

$$Lc := 64.282 \text{ kip}$$

$$Ld := 4.475 \text{ kip}$$

Note: data shown corresponds
to a loaded Hyster H300HD

$$\text{wheelbase} := 129.9 \text{ in}$$

$$\text{len} := 20 \text{ ft}$$

$$\text{lenC} := 9 \text{ ft}$$

$$\text{lenD} := \text{lenC} + \text{wheelbase}$$

$$\text{lenD} = 19.825 \text{ ft}$$

Calculate the reactions at A and B:

$$Rb := \frac{Lc \cdot \text{lenC} + Ld \cdot \text{lenD}}{\text{len}} \quad Rb = 33.3627 \text{ kip}$$

$$Ra := Lc + Ld - Rb \quad Ra = 35.3943 \text{ kip}$$

Calculate the maximum shear forces:

$$\text{posVmax} := Ra \quad \text{posVmax} = 35.3943 \text{ kip}$$

$$\text{negVmax} := Rb \quad \text{negVmax} = 33.3627 \text{ kip}$$

Calculate the maximum bending moment:

$$M_{\text{max}} := \text{posVmax} \cdot \text{lenC}$$

$$M_{\text{max}} = 3.1855 \cdot 10^5 \text{ ft lbf}$$

Recalculate allowable bending moment using yield strength

$$M_{\text{all}} := S_{\text{mod}} \cdot \sigma_{\text{all}}$$

$$M_{\text{all}} = 3.7706 \cdot 10^5 \text{ ft lbf}$$

Compare maximum bending moment to allowable bending moment:

```

if Mall > Mmax
  result := "Pass"
else
  result := "Fail"

```

result = "Pass"

Calculate Max Deflection:

E = modulus of elasticity (ksi)
 I = moment of inertia about horizontal centroidal axis (in⁴)
 ymaxC = maximum deflection at C from load C only (in)
 xC = position of maximum deflection (ft) measured from point A
 θa = angle of deflection at A from load D only (radians)
 yD = deflection at xC from load D only (in)
 ymax = maximum deflection (in)

Define modulus of elasticity and moment of inertia:

$$E := 29000 \text{ ksi}$$

$$I := 4216.4402 \text{ in}^4$$

Calculate the maximum deflection at C from load C only:

$$y_{\max C} := \frac{-L_C \cdot \text{len}_C}{3 \cdot E \cdot I \cdot \text{len}} \left(\frac{\text{len}^2 - \text{len}_C^2}{3} \right)^{\frac{3}{2}} \quad y_{\max C} = -0.1494 \text{ in}$$

Calculate the position of the point of maximum deflection:

$$x_C := \text{len} - \left(\frac{\text{len}^2 - \text{len}_C^2}{3} \right)^{\frac{1}{2}} \quad x_C = 9.6882 \text{ ft}$$

Calculate the angle of deflection at A from load D only:

$$\theta_a := \left(\frac{(-L_d) \cdot \text{len}_D}{6 \cdot E \cdot I \cdot \text{len}} \right) \cdot (2 \cdot \text{len} - \text{len}_D) \cdot (\text{len} - \text{len}_D) \quad \theta_a = -3.0739 \cdot 10^{-6}$$

Calculate the reaction at A if only load D existed:

$$R_a := \frac{L_d \cdot (\text{len} - \text{len}_D)}{\text{len}} \quad R_a = 0.0392 \text{ kip}$$

Calculate the deflection at xC if only load D existed:

if $x_C > \text{len}_D$

$$y_D := \theta_a \cdot x_C + \frac{R_a \cdot x_C^3}{6 \cdot E \cdot I} - \frac{L_d}{6 \cdot E \cdot I} \cdot (x_C - \text{len}_D)^3$$

else

$$y_D := \theta_a \cdot x_C + \frac{R_a \cdot x_C^3}{6 \cdot E \cdot I}$$

$$y_D = -2.7351 \cdot 10^{-4} \text{ in}$$

Due to the principle of superposition deflections "ymaxC" and "yD" may be added to obtain the total maximum deflection at xC:

$$y_{\max} := y_D + y_{\max C}$$

$$y_{\max} = -0.1497 \text{ in}$$

References:

Mechanics of Materials, 2nd ed. by Beer and Johnson, pg. 446-48

Formulas for Stress and Strain, 5th ed. by Roark and Young, pg. 96-97